A Study of the Effect of the Wheel Load, Tire Dimensions and Water Depth on the Vehicle Critical Speed in Wet Roads

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Abstract
A study of the critical speed of the vehicles on the wet roads has been done. And how it is affected by the following parameters: wheel load, tire width, tire radius and water layer depth and also the nature of the contact area of the tire (grooved or smooth).

It was found that the wheel load increase the critical speed positively while the tire width, the tire radius and the water layer depth decreased the critical speed. It was also found that grooves in the tire surface improve vehicle performance on wet roads.

Kay Word: Critical speed of the vehicle, Road parameters, Tire parameters

Introduction
Hydroplaning is a major safety concern in wet-weather driving which occurs when the traveling speed of a vehicle becomes so high that the hydrodynamic pressure of the water between its tires and the pavement surface rises to a critical value. When this condition prevails, the tires would be supported by the water film and the driver may lose the braking and the steering control of the vehicle[1]. Statistics studies that cover various parts of the world indicate that is approximately 20% of all the road traffic accidents occur due to wet weather conditions[2,3]. Although there are no detailed statistics on the exact causes of the wet-weather accidents, it is believed that low skid resistance and hydroplaning are major factors leading to
the accidents:\cite{1,4,5}. Hydroplaning refers to a situation in which the presence of water film in the tire-and-pavement contact region significantly reduces the frictional resistance at the interface, and this results in the skid resistance and vehicle steering control.

On the road surface with a known thickness of the water film, the factors that influence the vehicle hydroplaning or critical speed (i.e. vehicle speed at which the hydroplaning occurs) including the tire related factors and the pavement related factors. The main tire related factors are the tire inflation pressure, the wheel load, the tread depth and the tire type. For instance, increasing the tire inflation pressure, the wheel load or the tire tread depth will raise the critical speed. Hence reducing the hydroplaning risk:\cite{3,6}.

The main pavement related factors affect the hydroplaning or critical speed are: surface micro texture, macro texture nature and the pavement cross-slope. Increasing the pavement cross-slope facilitates drainage, resulting a thinner water film thickness on the pavement surface and higher hydroplaning or critical speed:\cite{7}.

**The Pavement Parameters Used In This Study**

The parameters adopted in the analytical hydroplaning that used in this study model are presented in this section.

**Pavement Surface Model**

The pavement surface model used in this study is that adopted in refs:\cite{1,8,9,10,11}. This model considers a smooth plane pavement surface for all the analysis and this represent the worst case and a conservative estimation of the critical speed for in-service pavements, and this is presented in table (1).

**Water Film Properties**

The properties of the water film that covers the road (at 20°C temperature) used in this study are: The density, dynamic viscosity and kinematic viscosity of water are 998.2 kg/m$^3$, 1.002 x 10$^{-3}$ Ns/m$^2$ and 1.004 x10$^{-6}$ m$^2$/s respectively:\cite{12}.

**Analytical Approach**

Reynolds equation has been used to analyse the parameters and assess the performance of the operation. The contact region between the tire and the road (fig.(1)) looks like the convergence half of the conventional bearing. Therefore Reynolds equation of convergence and squeezing terms in the right hand side has been used this from is:\cite{13}:

$$\begin{align*}
\frac{\partial}{\partial x} \left[ h^3 \frac{\partial P}{\partial x} \right] + \frac{\partial}{\partial z} \left[ h^3 \frac{\partial P}{\partial z} \right] = 6U \left[ \frac{\partial h}{\partial x} \right] + 12 \frac{\partial h}{\partial t} \ldots (1)
\end{align*}$$

Assuming that $\frac{\partial h}{\partial z} = 0$. And considering the viscosity is constant over the whole contact region, then expanding Reynolds equation to give:

$$\begin{align*}
h^3 \frac{\partial^2 P}{\partial x^2} + 3h^3 \frac{\partial h}{\partial x} \frac{\partial P}{\partial x} + h^3 \frac{\partial^2 P}{\partial z^2} + 6U \frac{\partial h}{\partial x} + 12 \frac{\partial h}{\partial t} \ldots (2)
\end{align*}$$

Reynolds equation has been solved numerically using the finite difference technique. And this was achieved by dividing the contact region into (m) number of grids annually and (n) number of grids axially as shown in fig (1). A reasonable accuracy was achieved in the implementation of the computer program that based on the finite difference model. This was achieved by using (m x n) equal (48 x 128).

Modeling equation (2) by using the finite difference technique of five nodes scheme gives:

$$D_1 P_{i+1,j} + D_2 P_{i-1,j} - D_3 P_{i,j} + D_4 P_{i+1,j+1} + D_5 P_{i-1,j-1} = D_6 \ldots (3)$$

Solving equation (3) using the iteration technique gives the water film pressure at all the points in the annual and axial directions in the contact region. And this was achieved by using the matrix method Gaussian elimination:\cite{14} (by the computer program) in solving the simultaneous equations, which represent all the nodes.

**Results And Discussion**

The program results were obtained and the performance characteristics were monitored by drawing the following relationships.

The pressure variation annually is presented in fig (2). This figure shows the same behavior of the oil film pressure on the bearing application. Noting that in this
application the pressure profile has a sharp raise to give the peak. And this is due to the nature of the tire geometry.

Fig (3) shows the water film pressure variation axially. The pressure profile is chopped into many portions depending on the number of the annual grooves. Any way this technique (using the annual grooves) helps in raising the critical speed of the vehicle, so this type of tires usually are used over the raining seasons. While the smooth surface tire has a uniform pressure profile, and this gives a lower critical speed, therefore it is imp referable to be used over the raining seasons.

**The Effect Of The Tire Width**

Figure (4) shows the relationship between the critical speed of the vehicle and the tire width for two types of tires. These types are, 1st, with annual grooves and the 2nd is for smooth surface tire. Generally, it is clear from the figure that the tire width effects the critical speed of the vehicle adversely for both types of tires. And this means that the narrow tires is safer than the one with a large width to be used in the wet roads, and this is well justified on the bases of the pressure, area and force relation. Also this figure shows that using the tire annually grooved is safer than that of smooth surface. This is because that the groove drain the water and break the water film pressure and thus preventing build up high pressure in the water film, which lift the tire and losing the vehicle control.

**The Effect Of The Tire Radius**

The relation between the critical speed of the vehicle and the tire radius for smooth and grooved tires are presented on figure (5). Generally, the tire radius effect the vehicle critical speed adversely (as the tire width effect). And this due to the fact that; as the radius increased as the surface flat end and thus the contact area increased which result higher force, and that lift the tire early. Also this figure shows that the grooves improve the vehicle tire performance by increasing the critical speed and make the driving on a wet roads safer. This is due to draining the water and breaking the pressure profile.

**The Effect Of The Wheel Load**

Figure (6) shows the relationship between the vehicle critical speed and the wheel load, for both smooth and grooved tires. This figure shows that increasing the wheel load has a positive effect on the critical speed, i.e., increasing it. And this is due to requiring a larger lifting force, and this require a higher water film pressure, and this couldn't be achieved at low vehicle speed. Also from this figure, it is clear that the tire grooves improve the operation performance (increasing the critical speed) because it help in draining the water and breaking the pressure profile, and this have the same behavior and trends of ref [15] figures (4.12)(4.15).

**The Effect Of The Water Layer Thickness**

Figure (7) shows the relationship between the critical speed of the vehicle and the depth of the water layer on the road, for smooth and grooved tires. From this figure it is clear, that, generally, increasing the depth of the water layer decreasing the critical speed. And this due to increasing the contact area between the tire and the water. And also it could be seen that the effect of the water layer depth, from small values of depth is much higher than that of the large values of the water depth. And this is well justified on the bases of the convergence zone shape, which has little effect when the water film thickness becomes large. Also it could be noticed that the effect of the grooves, for small values of water layer, depth is larger than its effect on the case of large value of water layer depth. This is due to the blockage of the water passage by the water. But another adverse factor could raise and may need to be considered carefully. This factor is the water wedges which has a great effect in the case of large value of water layer depth.

**Conclusions**

From the results of this study, the following conclusions may be drawn.

1. The heavy vehicle performance is safer than the light vehicle in the wet roads.
2. Increasing the width, the radius or both has adverse effect on the vehicles performance in the wet roads.
3. A road with large value of water depth is more risky than that of small values of water layer depth.
4- Using the grooved tires, especially with random shapes almost overcome the wet road problems.

References


6. Mosher, L. G., 1969, Results from studies of highway grooving and texturing by several state highway departments: Pavement traction and grooving studies. NASA SP-5073, National Aeronautics and Space Administration, Washington, D.C.


Fig. (1) (a) Tire geometry, (b) contact region shape, (c) contact region divided into annual and axial grids
Fig. (2) The water film pressure \( (P) \) variation annually

Fig. (3) The water film pressure \( (P) \) variation axially

Fig. (4) Critical Speed Variation With The Tire Width

Fig. (5) Critical Speed Variation With the Cross Sectional Radius
Table (1): Parameters used in the analysis

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Details</th>
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<tbody>
<tr>
<td>Passenger car tire</td>
<td>ASTM E 501 standard G78-15 tire</td>
</tr>
<tr>
<td>Tire analyzed</td>
<td>Smooth tire, Longitudinally grooved tire</td>
</tr>
<tr>
<td>Pavement surface</td>
<td>Smooth plane surface</td>
</tr>
<tr>
<td>Wheel load</td>
<td>3.924, 4.4145, 4.905, 5.3955 and 5.886 KN</td>
</tr>
<tr>
<td>Cross Section Radius</td>
<td>280, 300, 320, 340 and 360 mm</td>
</tr>
<tr>
<td>Tire width</td>
<td>140, 160, 180, 200 and 220 mm</td>
</tr>
<tr>
<td>Tire groove width</td>
<td>8 mm</td>
</tr>
<tr>
<td>Tire groove depth</td>
<td>8 mm</td>
</tr>
<tr>
<td>Center-to-center spacing</td>
<td>20 mm</td>
</tr>
<tr>
<td>Water depth</td>
<td>10, 20, 30, 40 and 50 mm</td>
</tr>
</tbody>
</table>

Fig. (6) Critical Speed Variation With wheel load

Fig. (7) Critical Speed Variation With The water Layer Thickness