

## *Experimental Investigation of the Effects of Some Operating Diesel Engine Variables on Emitted Particulate Matters (PM)*

Adel M. Saleh

Lecturer, Mechanical Engineering Department- University of Technology

### Abstract

The diesel engine is the most efficient prime mover commonly available today. Diesel engines move a large portion of the world's goods, power much of the world's equipment, and generate electricity more economically than any other device in their size range. But the diesel is one of the largest contributors to environmental pollution problems worldwide, and will remain so, with large increases expected in vehicle population.

This experimental study has been conducted with direct injection diesel engine and particulate matters (PM) concentrations were measured at variable operating variables. The results show that PM concentrations influence by changing equivalence ratio, load, engine speed and injection timing.

**Key words:** PM, Equivalence Ratio, Speed, Injection Timing, Load

### دراسة عملية لتأثير بعض المتغيرات التشغيلية لمحرك ديزل على السناج المنبعث

الخلاصة

يعد محرك الديزل من أعلى المحركات الأولية المتوفرة اليوم كفاءة، إذ تعمل محركات الديزل في نقل جزء كبير من بضائع العالم، وتجهز قدرة لمعظم الأجهزة، كما تولد طاقة كهربائية اقتصادية أكثر من أي جهاز آخر في مدى حجمها. ولكن محركات الديزل هي أحد أعظم المساهمين في مشاكل التلوث البيئي حول العالم، وستبقى كذلك، مع الزيادة الواسعة في أعداد السيارات المتوقعة. تمت هذه الدراسة العملية بمحرك ديزل ذي حقن مباشر وتم قياس تراكيز المواد الدقائقية (السخام) في ظروف تشغيلية مختلفة. بينت النتائج أن تراكيز المواد الدقائقية تتأثر بالتغير في النسبة المكافئة والحمل و سرعة المحرك وتوقيت الحقن.

الكلمات الدالة: المواد الدقائقية، النسب المكافئة، توقيت الحقن، الحمل

### Nomenclatures

PM	particulate matters	$Q_t$	elementary and final air flow rate through the device ( $m^3/sec$ ).
CO	carbon monoxide	$t$	sampling time in (min).
HC	unburnt hydrocarbons	$w_1$	filter weight before sampling operation in (g).
bp	brake power	$w_2$	filter weight after sampling operation
bmep	brake mean effective pressure		
CN	Cetane Number		
$V_t$	drawn air total volume ( $m^3$ )		

### Introduction

Like any other internal-combustion engine, diesel engines convert the chemical energy contained in diesel fuel

into mechanical power. Diesel fuel is injected under pressure into the engine cylinder, where it mixes with air and combustion occurs. The lean nature of the diesel-air mixture results in a cooler

combustion environment with smaller volumes of carbon monoxide (CO) and hydrocarbons (HC). However, diesel engines emit a complex mixture of air pollutants, composed of gaseous and solid material. The visible emissions in diesel exhaust are known as particulate matter (PM), which includes carbon particles or "soot" <sup>[1 & 2]</sup>. Diesel exhaust also contains a variety of harmful gases and over 40 other known cancer-causing substances <sup>[3]</sup>.

While the operational advantages of diesel engines are clear, diesel fuel is a major contributor to particulate matter (PM). Diesel particulate emissions are of increasing concern as they are small, often less than 10 microns in size, and consist of a complex mix of engine oils, sulfates and inorganic materials. These particles have been identified by health experts as contributing to a variety of lung related illnesses including asthma, emphysema and bronchitis. US Protection Agency identified diesel PM as a "likely human carcinogen," and followed this with new stringent standards aimed at reducing emissions from on-road vehicles by as much as 90 percent <sup>[4 & 5]</sup>.

Smoke may be defined as particles, either solid or liquid (aerosols), suspended in the exhaust gases, which obstruct, reflect, or refract light <sup>[6]</sup>. Diesel engine exhaust smoke can be categorized under two headings:

1. Blue/white in appearance under direct illumination, and consisting of a mixture of fuel and lubricating oil particles in an unburnt, partly burnt, or cracked state <sup>[7]</sup>.

2. Grey/black in appearance, and consisting of solid particles of carbon from otherwise complete combustion of fuel. The blue component derives mainly from an excess of lubricating oil in the combustion chamber, resulting from deterioration of piston ring sealing, or valve guide wear, and is thus an indication of a need for mechanical

overhaul. However unburnt fuel can also appear as blue smoke. The white component, on the other hand, is mainly a result of too low a temperature in the combustion chamber during the fuel injection period <sup>[8]</sup>.

Fuel properties are also capable of influencing smoke emissions. Thus, increasing the cetane number will reduce the tendency to produce white smoke, as also will increased volatility, usually indicated by reduction in mid-boiling point. On the other hand, chemical composition, cetane number and volatility all affect black smoke in a complex way, while increasing relative density will increase black smoke, for the same fuel pump setting, merely as a result of the increased mass of fuel injected <sup>[9]</sup>.

PMs are contributed to low load operation and large load swings causing unburnt fuel in the exhaust. Particle emissions are also influenced by the fuel ash and sulphur content as well as poor combustion due to insufficient engine preheating. Particle emissions from a diesel engine are typically low during steady state operation at higher loads, but during startup, low load operation, and large load swings, it is common to see a puff of black smoke from the exhaust stack. Smoke emissions draw attention in pristine areas, also some local regulations are now prohibiting smoke emissions during operation in coastal areas <sup>[10]</sup>.

The principle exhaust treatment technologies that have been successfully used to reduce diesel PM from diesel-fueled engines used in land-based applications are diesel particulate filters (DPF), Diesel oxidation catalysts (DOC), flow through filters (FTF) or combinations of technologies <sup>[11]</sup>.

The aim of this paper is to study practically the PM emitted from unmodified four cylinders direct

injection diesel engine fueled with conventional diesel fuel.

### Experimental Setup

Experimental apparatus of engine under study is direct injection, water cooled four cylinders, in-line, naturally aspirated FIAT diesel engine (Fig. 1) whose major specifications are shown in Table 1. The engine was coupled to a hydraulic dynamometer through which load was applied by increasing the torque.

The following equations were used in calculating engine performance parameters:

$$\text{Brake power} \\ bp = \frac{2\pi * N * T}{60 * 1000} \text{ kW} \quad \dots (1)$$

Brake mean effective pressure

$$bmep = bp \times \frac{2 * 60}{V_{sn} * N} \text{ kN/m}^2 \quad (2)$$

Conventional diesel fuel (CN=46.8) was operated on the engine; meanwhile combustion characteristics were measured and analyzed at the same brake mean effective pressure (bmep) and speed, to clarify the effect of engine variables on emitted PM emissions.

Low volume air sampler type Sniffer L-30 (Fig. 2) was used to collect emitted PMs. Whatmann-glass microfilters were used to collect PMs. These filters were weighted before and after the end of sampling operation which extend for one hour. PMs concentrations were determined by the equation:

$$PM \text{ in } (\mu\text{g/m}^3) = \frac{w_2 - w_1}{Vt} \times 10^6 \quad \dots (3)$$

Where:  $PM$  = particulate matters concentration in ( $\mu\text{g/m}^3$ ).

$w_1$  = filter weight before sampling operation in (g).

$w_2$  = filter weight after sampling operation in (g).

$Vt$  = drawn air total volume ( $\text{m}^3$ )

$Vt$  can be found by the equation:

$$Vt = Q_i \cdot t \quad \dots (4)$$

Where:

$Q_i$  = elementary and final air flow rate through the device ( $\text{m}^3/\text{sec}$ ).

$t$  = sampling time in (min).

Each filter was put in plastic bag temporarily at the end of collecting samples operation until analyzing and studying the results using light microscope.

### Results and Discussion

Fig. 4 shows the effect of equivalence ratio on emitted PM at constant speed 1500 rpm and medium load ( $44 \text{ kN/m}^2$ ). Emitted PM was high at very low equivalence ratio ( $\phi \leq 0.3$ ). The range on the minimum PM concentration was ranged between ( $0.3 \leq \phi \leq 0.6$ ) that produced the higher brake power. At equivalence ratios ( $\phi \geq 0.6$ ) PM concentrations start to increase highly, due to incomplete combustion caused by improper mixing accompanied with increasing fuel quantity.

Load effect on PM concentration at constant speed was studied as Fig. 5 represents. PM concentrations reduced from low to medium loads. For loads in the range of  $20\text{-}60 \text{ kN/m}^2$  the concentrations tend to be stable. At loads higher than  $60 \text{ kN/m}^2$  PM concentrations increased significantly. At low loads the combustion chamber temperature is low, which lead to bad combustion especially for higher hydrocarbon molecules resulting in higher PM concentration. At medium loads the chamber temperature suitable and adequate combustion led to this approximate stability. At high loads, more fuel was injected to maintain engine speed, accompanied with higher combustion chamber temperatures causing higher PM concentrations.

PM concentration increased at low and high speeds, and reached it

minimum values at medium speeds, as Fig. 6 represents. The high concentration of PM is due to reduction in volumetric efficiency at low speeds. At high speeds the air-fuel preparation time reduced highly, giving higher PM concentrations.

Injection timing effect on emitted PM was studied as Fig. 7 shows. Retarding injection timing reduced the available time for air – fuel mixture preparation producing high PM concentration. Advancing injection timing increased preparation time and contain fuel delay period producing better combustion with less PM concentration. This is right for working without knock. Advancing injection timing was limited by engine appearance. In this work the knock phenomenon effects on PM concentration were not investigated.

### Conclusions

- 1- PM concentrations emitted from diesel engine depend on many design and operating variables.
- 2- Working at equivalence ratios that give the maximum brake power values produce lower PM concentrations.
- 3- Working at low or high equivalence ratios produce higher PM concentrations.
- 4- Engine operation at medium loads gives the minimum PM concentrations values.
- 5- Engine operation at low or high loads gives higher PM concentrations.
- 6- Low and high speeds produce high PM concentrations, while medium speeds produce lower concentrations.
- 7- Retarding injection timing causes high PM concentration; on the contrary, advancing injection timing results in lower concentrations.

### References

1. Eldering A, Cass GR. Source-oriented model for air pollutant effects on

visibility, *J. of Geophys. Res.*, 101 (D14), 9,343-19,369, 1996.

2. Labhsetwar N K, Biniwale R B, Kumar R, Bawase m A, Rayalu S S, Mitsuhashi T and Haneda H, Application of catalytic materials for diesel exhaust emission control, *Current sci.*, vol. 87, No. 12, 2004.
3. Garshick E, Laden F, Hart J E, Rosner B, Smith T J, Dockery D W and Speizer F, Lung Cancer in Railroad Workers Exposed to Diesel Exhaust. *Environ Health Perspect* vol. 112, pp: 1539–1543, 2004.
4. Dreier T, Bougie B, Ganippa L, Dam N, Gerber T and Meulen J T, Modeling of time-resolved laser-induced incandescence (TIRE-LII) transients for particle sizing in high-pressure spray combustion environments, *Proceedings of the International Bunsen Discussion Meeting 2005: Laser-induced Incandescence, Quantitative interpretation, modeling, application*, 2005.
5. Livanos G, Kanellopuloue and. Kyrtato N P, Marine Diesel Engine Rapid Load Acceptance without Smoke Emissions, *Proceedings of the 7th International Symposium on Marine Engineering Tokyo*, October 24th to 28th, 2005
6. U.S. Environmental Protection Agency (EPA). Air Pollution Control Technology Fact Sheet: Flue Gas Desulfurization (FGD) – Wet, Spray, Dry, and Dry Scrubbers. EPA-452/F-03-034. July 7, 2003.
7. Allansson F and et al. European Experience of High Mileage Durability of Continuously Regenerating Diesel Particulate Filter Technology; SAE Technical Paper Series, 2000-01-0480. March 2000.
8. Avol E L, Gauderman W J, Tan S M, London S J and Peters J M.

- Respiratory effects of relocating to areas of differing air pollution levels. Amer. J. of Resp. and Crit. Care Med. Vol. 164, pp: 2067-2072, 2001.
9. Khair M and McKinnon D L, Performance Evaluation of Advanced Emission Control Technologies for Diesel Heavy-Duty Engines, SAE 1999-01-3564; 1999.
10. Gomaa M, Alimin A J and Kamarudin K A, Trade-off between NO<sub>x</sub>, Soot and EGR rates for an IDI diesel engine fuelled with JB5, World Academy of Science, Engineering and Technology, vol. 62, pp: 522-527, 2010.
11. Oh S K, Baik D S and Han Y C, Performance and exhaust gas characteristics on diesel particulate filter trap, International Journal of Automotive Technology, Vol. 3, No. 3, pp: 111-115, 2002.



**Fig. 1, photographic picture of the experimental rig. Fig. 2, drawing air equipment to collect PM type Sniffer**



Fig. 3, light microscope used to study on PM specifications

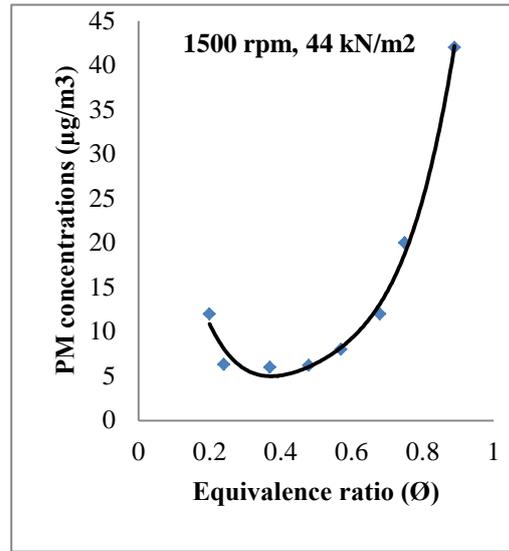


Fig. 4, Wide range of equivalence ratios effect PM concentration at 1500 rpm and medium load.

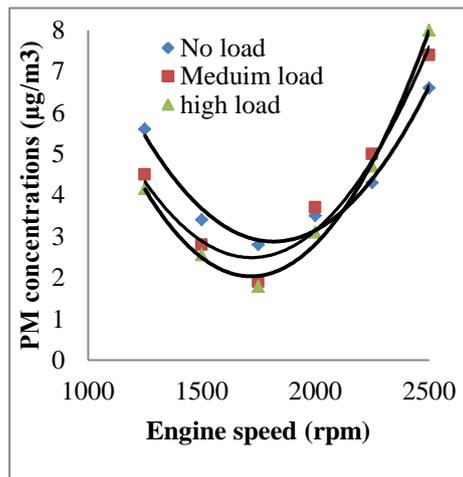


Fig. 5, Load effect on PM concentrations at 1500 rpm and  $\phi=0.55$

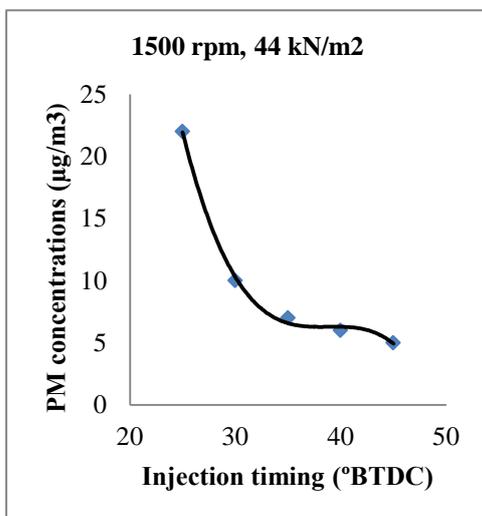


Fig. 6, Engine speed effect on PM concentrations at variable loads.

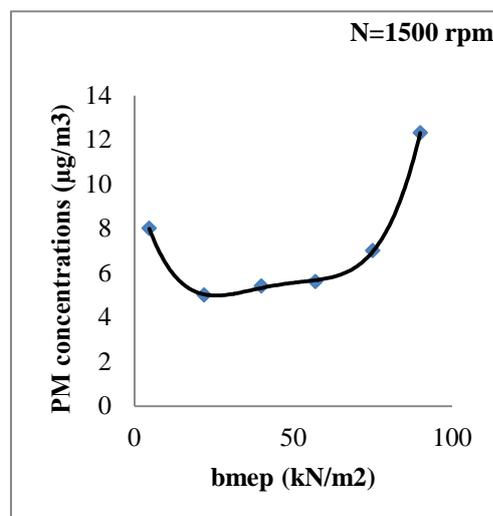


Fig. 7, Injection timing effect on PM concentration at constant engine speed (1500 rpm) and medium load.

